# Yielding of Coarse-Fine Particle Mixtures in Mineral Slurries

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## **Particle Mixtures**

# Industries

- Water/Wastewater
- Algae for Biofuels
- Desalination
- Minerals Processing
- Ceramics
- Pulp and Paper
- Blood

and many more

# Processes

• Flow

**Pumping and Mixing** 

• Dewatering

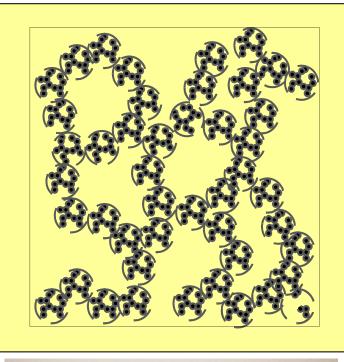
Thickeners, Filters, Centrifuges

- Theory & Methods
- Shear Rheology
- Compressional Rheology



#### **Material Properties**

- Gel Point,  $\phi_g$ 
  - Minimum solids volume fraction at which the suspension forms a continuously networked structure that transmits its weight to the suspension below.
  - Can make an approximate measure from a batch settling experiment.

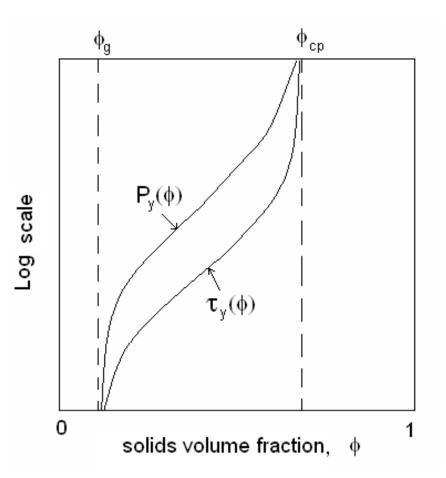






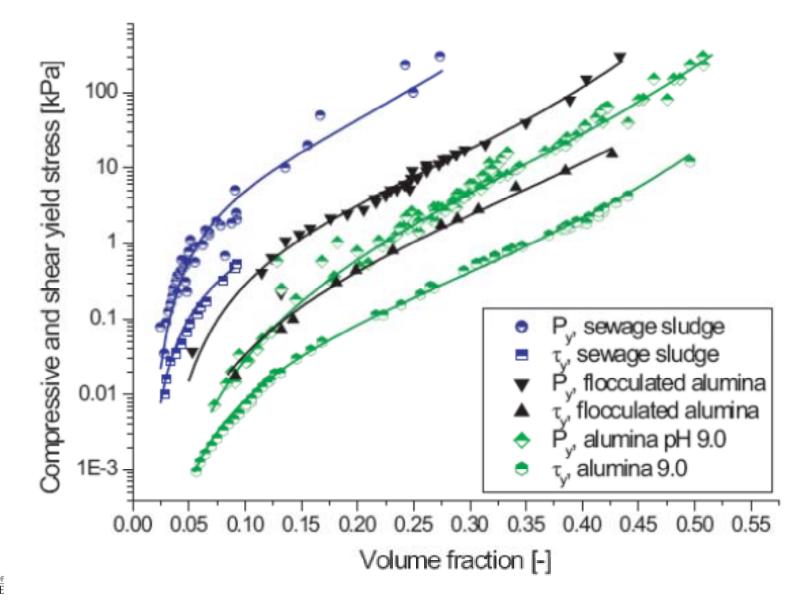
#### **Material Properties**

- Compressive Yield Stress,  $P_y(\phi)$ 
  - Minimum compressive force required for a suspension to yield and compress.
- Shear Yield Stress,  $\tau_y(\phi)$ 
  - Minimum shear force required for a suspension to yield and flow.

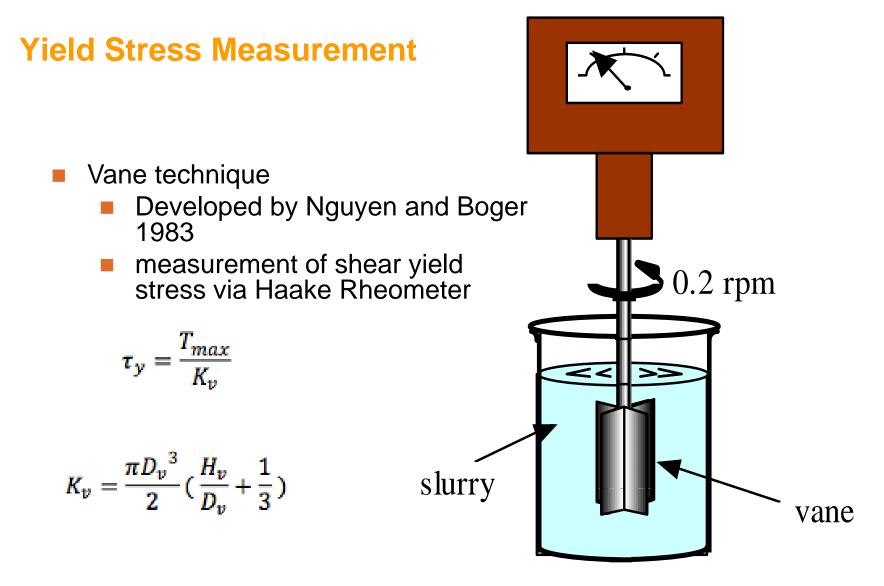




#### **Material Properties**







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- Nguyen QD, Boger DV, Journal of Rheology, 29 (1985) 335-347
- Pashias N, Boger DV, Summers J, Glenister DJ, Journal of Rheology, 40 (1996) 1179-1189

# **Poly-disperse mixtures**

| Particle Size Distribution   | <ul> <li>Bi-disperse mixtures</li> <li>Poly-disperse mixtures</li> </ul>   |  |
|--|--|--|
| Determination of bi-<br>disperse mixture<br>properties               | <ul> <li>Measurements</li> <li>Equilibrium Batch Settling</li> <li>Yield stress measurement</li> <li>Shear rheology measurements</li> <li>Model development</li> </ul> |  |
|  |  |  |
| Development of an<br>industrial tool for<br>prediction of properties | <ul> <li>What is the minimum required information?</li> </ul>  |  |



## **Materials - Solids**

- Alumina
  - AKP-50 (4000 kg m<sup>-3</sup>, d<sub>50</sub> 0.14 μm, IEP 9.2)
- Calcium Carbonate
  - Omyacarb-2 (2700 kg m<sup>-3</sup>, d<sub>50</sub> 3.5 μm, IEP 8)
  - Omyacarb-40 (2700 kg m<sup>-3</sup>, d<sub>50</sub> 32.5 μm, IEP 8)
- Sand
  - AKP-50 (2600 kg m<sup>-3</sup>, d<sub>50</sub> 1083 μm)

#### **Materials - Electrolyte**

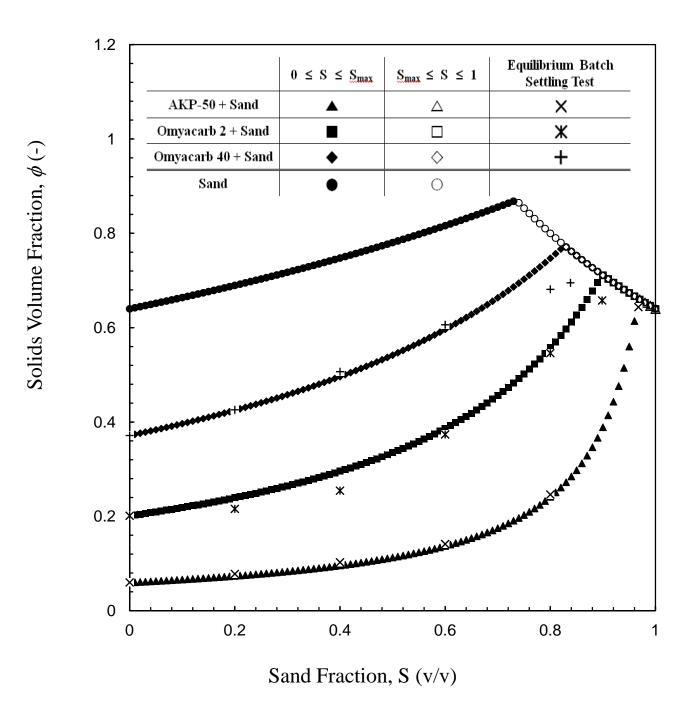
- Potassium Nitrate Solution
  - 0.01 M KNO<sub>3</sub> (aq) at pH 9.2



## **Gel Point (Bi-disperse mixtures)**

1.2 Measured Equilibrium Batch  $0 \le S \le S_{max}$  $S_{max} \le S \le 1$ Settling Test Vane technique AKP-50 + Sand  $\triangle$ х ж Omyacarb 2 + Sand Solids Volume Fraction,  $\phi(-)$ + Omyacarb 40 + Sand  $\diamond$ Ο Sand **Predicted** 0.8 Mixture solids volume fraction  $\phi_{(mixture)} = \phi = \phi_{(fine)} + \phi_{(coarse)}$ 0.6 Coarse fraction  $S = \frac{\phi_{(coarse)}}{\phi_{(mixture)}} = \frac{\phi_{(coarse)}}{\phi_{(fine)} + \phi_{(coarse)}}$ 0.4 0.2 Predictions  $\phi_{g_{(mixture)}} = \frac{\phi_{g_{(fine)}}}{1 - S + S\phi_{g(fine)}}, \quad 0 \le S \le S_{(max)}$ 0 0.2 0.4 0.6 0.8 1 0 Sand Fraction, S (v/v) $\phi_{g(mixture)} = \frac{\phi_{cp(coarse)}}{S}, \quad S_{(max)} \le S \le 1 \qquad \phi_g = \phi_{cp} = 0.64 \text{ for coarse sand}$ 







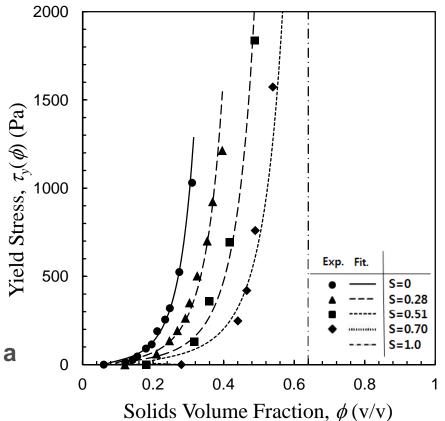
## **Yield Stress Constitutive Equation**

Yield stress data is fitted to a constitutive equation:

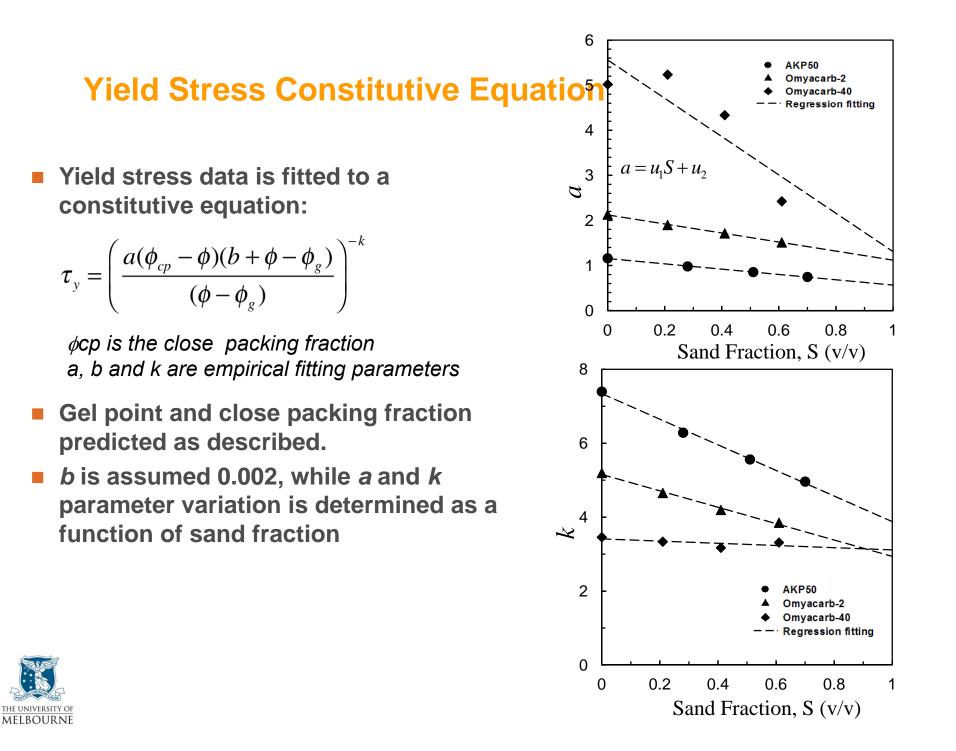
$$\tau_{y} = \left(\frac{a(\phi_{cp} - \phi)(b + \phi - \phi_{g})}{(\phi - \phi_{g})}\right)^{-k}$$

 $\phi$ cp is the close packing fraction a, b and k are empirical fitting parameters

- Gel point and close packing fraction predicted as described.
- b is assumed 0.002, while a and k parameter variation is determined as a function of sand fraction





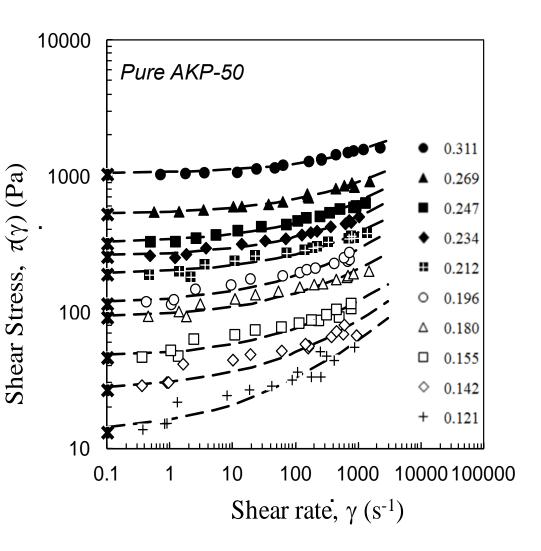


## **Herschel Bulkley model**

- Shear stress versus shear rate data also determined using the vane
- Data is fitted to Herschel Bulkley equation

 $\tau = \tau_y + k \dot{\gamma}^m$ 

- Yield stress determined using prediction method
- k and m fitted to data
  - Again, can determine variation of parameters with coarse fraction.





# **Sedimentation and Segregation**

Particles settle due to gravity, even when the solids concentration is greater that the gel point.

Larger particles can settle faster.

- Stokes Law
  - For isolated particles.
  - Gives maximum potential rate of segregation

$$V_{coarse} = \frac{d_{coarse}^2 \cdot \Delta \rho \cdot g}{18\eta}$$

$$\Delta \rho_{\text{fine,suspension}} = \phi_{\text{fine}} \rho_{\text{fine}} + (1 - \phi_{\text{fine}}) \rho_{\text{medium}}$$

where  $V_{\text{coarse}}$  = the velocity of coarse particle  $d_{\text{coarse}}$  = the diameter of coarse particle  $\Delta \rho$  = the density difference between coarse particle and fine particle suspension g = the acceleration due to gravity  $\eta$  = the viscosity of fine particle suspension at a given shear rate

10000



# Conclusions

Rheology of bi-disperse mixtures can be predicted:

- $\phi_g$  and  $\phi_{cp}$  variations can be predicted for bi-disperse mixtures
  - based on pure component properties,
  - requires significant particle size difference.
- $\tau_v$  and  $P_v$  variations can be predicted
  - uses a constitutive equation.
- $\tau$  versus  $\dot{\gamma}$  variations can be predicted
  - using Herschel Bulkley parameters that vary with mixture composition.
- Sedimentation and segregation can compromise measurements
  - Timescale of segregation must be longer than that of measurement.



## **Further Work**

- Polydisperse mixtures:
  - $\phi_g$  and  $\phi_{cp}$  can be accurately predicted for mixtures of 3 or more components, provided that particle size differences are significant.
  - The challenge is to quantify the impact of particle size distribution overlap.
- Dewatering:
  - Compressive yield stress,  $P_y(\phi)$  variations can be similarly be predicted for mixtures.
  - Settling rate predictions...



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